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# The influence of cuttlebone on the target strength of live golden cuttlefish (*Sepia esculenta*) at 70 and 120 kHz

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## Abstract

To quantitatively estimate the influence of cuttlebone on the target strength ( $TS$ ) of golden cuttlefish, the cuttlebone was carefully extracted from 19 live cuttlefish caught using traps in the inshore waters around Geoje-do, Korea, in early May 2010 and the  $TS$  was measured using split-beam echosounders (Simrad ES60 and EY500). The  $TS$ -length relationships for the cuttlefish (before the extraction of cuttlebone, Fish Aquat Sci. 17:361–7, 2014) and the corresponding cuttlebone were compared. The cuttlebone length ( $L_b$ ) ranged from 151 to 195 mm (mean  $L_b = 168.3$  mm) and the mass ( $W_b$ ) ranged from 29.3 to 53.2 g (mean  $W_b = 38.8$  g). The mean  $TS$  values at 70 and 120 kHz were  $-33.60$  dB (std = 1.12 dB) and  $-32.24$  dB (std = 1.87 dB), respectively. The mean  $TS$  values of cuttlebone were 0.19 dB and 0.04 dB lower than those of cuttlefish at 70 and 120 kHz, respectively. For 70 and 120 kHz combined, the mean  $TS$  value of cuttlebone was  $-32.87$  dB, 0.11 dB lower than that of cuttlefish ( $-32.76$  dB). On the other hand, the mean  $TS$  value of cuttlebone predicted by the regression ( $TS_b = 24.86 \log_{10} L_b - 4.86 \log_{10} \lambda - 22.58$ ,  $r^2 = 0.85$ ,  $N = 38$ ,  $P < 0.01$ ) was  $-33.10$  dB, 0.04 dB lower than that of cuttlefish predicted by the regression ( $TS_c = 24.62 \log_{10} L_c - 4.62 \log_{10} \lambda - 22.64$ ,  $r^2 = 0.85$ ,  $N = 38$ ,  $P < 0.01$ ). That is, the contribution of cuttlebone to the cuttlefish  $TS$  determined by the measured results was slightly greater than that by the predicted results. These results suggest that cuttlebone is responsible for the  $TS$  of cuttlefish, and the contribution is estimated to be at least 99 % of the total echo strength.

**Keywords:** *Sepia esculenta* Target strength, Influence of cuttlebone, Tilt angle, Length dependence

## Background

Most aquatic animals, such as swimbladder fish and cuttlefish, maintain their depth in the sea by adjusting their average density to equal that of seawater using gas-filled organs that serve as a buoyancy tank (Denton and Gilpin-Brown 1961; Denton et al. 1961; Denton and Taylor 1964). These aquatic animals use essentially the same mechanism in their swimbladders and cuttlebones to achieve the buoyancy control needed to minimize energy consumption (Midtvedt et al. 2007). If the body density is higher than the surrounding water, the animal sinks. Similarly, aquatic animals of lower density float towards the surface. As long as the aquatic animal is not moving, this task is fairly simple, but aquatic animals move and as soon as the animal ascends or descends, the hydrostatic pressure changes. In swimbladder

fish, to compensate for this, gas must be rapidly secreted into the swimbladder while descending and removed while ascending (Denton and Gilpin-Brown 1961; Denton et al. 1961; Denton and Taylor 1964; Ffney et al. 2006). However, in cuttlefish, such problems of pressure change are avoided by enclosing the gas inside an incompressible chamber within the cuttlebone, the volume of which is unaffected by depth, and so cuttlefish maintain neutral buoyancy almost independent of depth (Sherrard 2000). Thus, the buoyancy mechanisms used by cuttlefish and swimbladder fish differ. The cuttlebone of cuttlefish comprises ~9 % of total body volume, but the swimbladder of fish only 4–6 % of total body volume (Denton and Gilpin-Brown 1961; Denton et al. 1961; Denton and Taylor 1964; Webber et al. 2000; Horne 2008; Sunardi et al. 2008). Foote et al. (Foote 1980a, 1980b, 1985; Foote and Ona 1985) indicated that the swimbladder is responsible for more than 90 % of the reflected sound energy from a fish. These facts suggest that the

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contribution of cuttlebone to the *TS* of cuttlefish may be larger than that of the swimbladder to the *TS* of fish, if the volume of cuttlebone does not change with depth. Other than our earlier study (Lee and Demer 2014), there has been no systematic attempt to determine the relationship between the *TS* and size of cuttlefish, especially the importance of cuttlebone to cuttlefish *TS*.

The objective of this study was to estimate the influence of cuttlebone on the *TS* of golden cuttlefish (*Sepia esculenta*), by comparing the *TS-L* relationships for cuttlebone and cuttlefish at 70 and 120 kHz.

**Methods**

**Echosounders and calibrations**

The acoustic and mechanical system for measuring the *TS* of cuttlebone is shown in Fig. 1 (Lee and Demer 2014). It comprised two split-beam echosounders (ES60 and EY500, Simrad, Norway) operating at 70 and 120 kHz, two split-beam transducers (half-power beamwidths = 11° and 7.1°, respectively) and a DC servomotor system (motor: BG90, Sung Shin, Korea; driver: KDC248H, KScontrol, Korea) to control the tilt angles of the cuttlebone during each acoustic transmission. A water-cooling system maintained the seawater at a temperature  $T = 18.0\text{ }^{\circ}\text{C}$  (confirmed by measurements before and near the end of the experiment). The two transducers were mounted adjacently facing sideways, with the center of

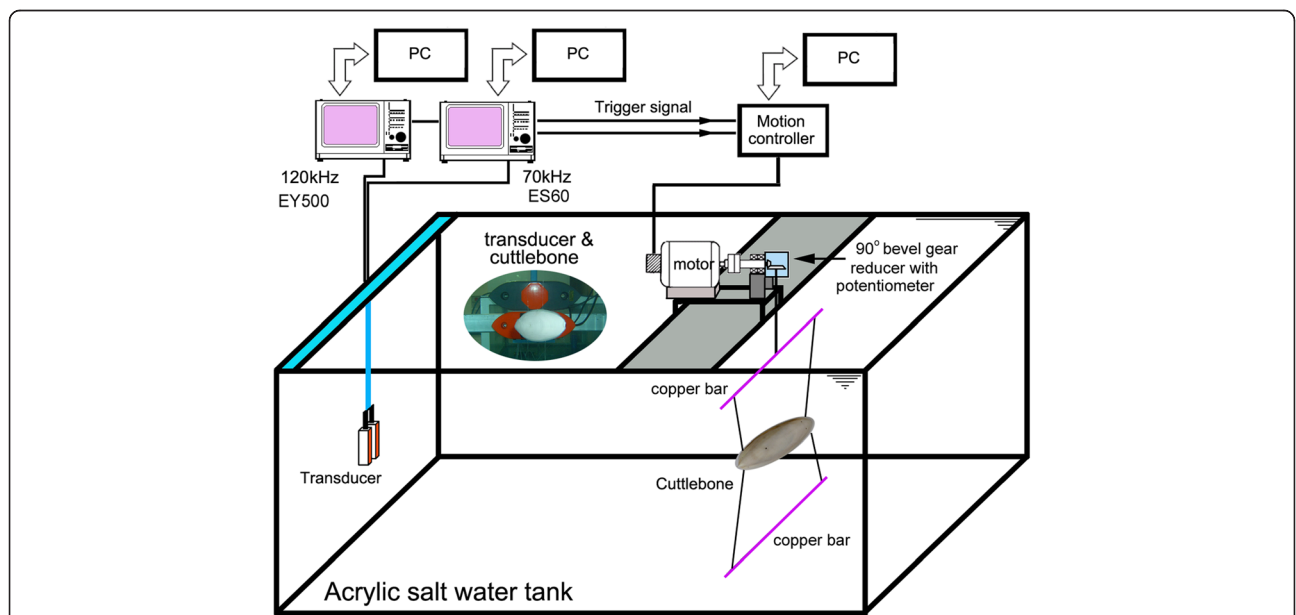
their faces at approximately 56 cm below the water surface.

Before and near the end of the experiments, the 70 and 120 kHz echosounders were calibrated using copper spheres of 32.1 and 23.0 mm diameter, respectively. The *TS* measurements were corrected for these calibrated offsets (−0.3 dB at 70 kHz and 0.5 dB at 120 kHz).

The experiment was conducted under the guidelines of Animal Ethics Committee Regulations, No. 554 issued from Pukyong National University, Busan, Korea. Nineteen cuttlebones directly extracted from 19 of the 23 live cuttlefish individuals (with the exception of four broken cuttlebones) tested in our earlier study (Lee and Demer 2014) were used as specimens for the *TS* measurements. Each cuttlebone was carefully extracted from each live cuttlefish specimen in sea water just before the experiment, and then immediately moved to a small tank filled with seawater at 18 °C.

To avoid variations in the acoustic and physical properties of the extracted cuttlebone with time, especially due to changes in shape, structure, chamber space and density, the cuttlebone *TS* measurement was rapidly performed under almost identical conditions, but in another acrylic salt-water tank, following measurement of the *TS* of live cuttlefish.

Before each set of measurements, the specimen was carefully suspended into the overlapping sound beams, avoiding the introduction of air bubbles. The tilt angle



**Fig. 1** Diagram of the acoustic-mechanical apparatus used to measure cuttlebone target strength (*TS*) versus length ( $L_b$ ), and tilt angle ( $\theta$ ). The apparatus comprise: a rectangular (1.2 width x 1.8 length x 1.2 m height), acrylic, saltwater tank; 70 and 120 kHz echosounders (Simrad ES60 and EY500, respectively); two split-beam transducers (Simrad ES70-11 and ES120-7 F, respectively); and a DC servo-motor system for controlling the tilt angle of cuttlebone. The cuttlebone was slowly rotated for the angle range of  $-90^{\circ}$  (head-down orientation) to  $90^{\circ}$  (head-up orientation) at a fixed speed of 0.167 rpm and stably maintained by tying monofilament lines between both ends of cuttlebone and two horizontal bars for suspending

of the cuttlebone was controlled using four monofilament lines (0.2 mm diameter), each tied to the anterior (head) and posterior (spine) parts of the cuttlebone, at both ends of an upper copper bar connected to the rotating axis of a DC servomotor system, and at both ends of a lower copper bar acting as a balancing weight (Fig. 1). The tilt angle was measured using a precision potentiometer (CP50, Sakae Tsushin Kogyo, Japan) connected to the axis of a 90° bevel gear reducer (ratio 240:1). The rotation speed of the cuttlebone was controlled by changing the input voltage of the DC servomotor system.

The definition of tilt angle for cuttlebone is shown in Fig. 2. The precise dorsal aspect of cuttlebone relative to the axis of the transducer was defined as a tilt angle of 0°, and the head up and down orientations relative to the center line of the cuttlebone were defined as positive  $\theta$  and negative  $\theta$  values, respectively.

In each case, the range between the transducers and the cuttlebone was approximately 1.2 m. The far-field ranges for the 70 and 120 kHz transducers (diameter  $d = 13.5$  and 12.9 cm) were  $\sim 0.47$  and  $\sim 0.68$  m (Lee 2006; Foote 2012), respectively. During the calibrations and the  $TS$  measurements, the 70 and 120 kHz echosounders transmitted 300 and 60 W pulses with durations of 256  $\mu$ s and 300  $\mu$ s every 0.2 s, and received the echoes using 6.2 and 12 kHz receiver bandwidths, respectively. The experiments in all cases were conducted using the same pulse duration, transmit power, pulse repetition interval and bandwidth used during the  $TS$  measurement of the calibration sphere. To avoid crosstalk, the measurements at 70 and 120 kHz were taken sequentially. When the trigger pulse of the echosounder was transferred to a PC-based motor controller (ComiSD501, Comizoa, Korea) and signal processor (ComiLX102, Comizoa, Korea), the  $TS$  measurement for the cuttlebone rotating at a fixed speed of 0.167 rpm, from the

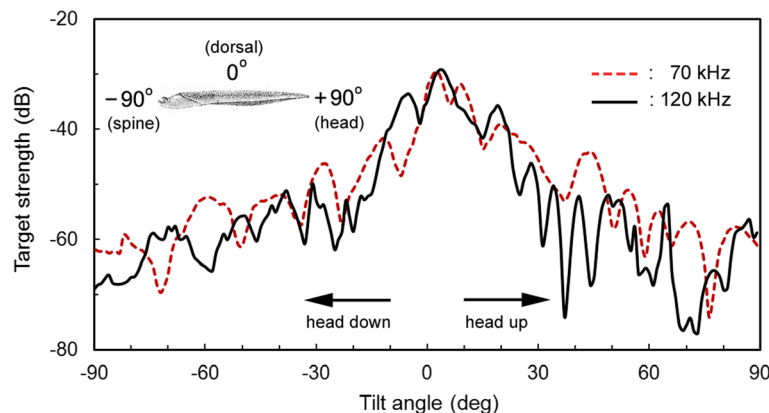
head-down orientation ( $-90^\circ$ ) to the head-up orientation ( $+90^\circ$ ), was conducted continuously. The output voltage of the precision potentiometer corresponding to the tilt angle and the echo data were recorded simultaneously and later processed to estimate the relationship between  $TS$  and tilt angle ( $\theta$ ) during each transmission. The echo data, logged by the echosounders, were post-processed using commercial software (Echoview V3.3, Sonar Data, Australia; EP500 v. 5.2, Simrad, Norway).

**Specimens and measurement of target strength**

The biological and morphological characteristics of 19 specimens of cuttlebone and the corresponding live cuttlefish (Lee and Demer 2014) used in the  $TS$  experiments are shown in Table 1. These characteristics—such as length, weight, width and thickness—were measured following completion of the acoustic experiments. Mantle length ( $L_c$ ) and body mass ( $W_c$ ) for cuttlefish ranged from 156 to 203 mm (mean  $L_c = 173.9$ ; deviation (std) = 13.10 mm) and 335–720 g (mean  $W_c = 527.4$ ; std = 104.4 g), respectively. The length ( $L_b$ ), weight ( $W_b$ ), width ( $W_d$ ) and thickness ( $T_h$ ) of cuttlebone ranged from 151 to 195 mm (mean  $L_b = 168.3$ ; std = 12.56 mm), 29.3–53.2 g (mean  $W_b = 38.8$ ; std = 7.23 g), 55–69 mm (mean  $W_d = 62.4$ ; std = 4.10 mm), and 13.6–18.0 mm (mean  $T_h = 15.7$ ; std = 1.24 mm), respectively.

The mean tilt angles ( $\langle\theta\rangle$ ) with standard deviations ( $S_\theta$ ) measured for 19 live cuttlefish at 70 and 120 kHz in our earlier study (Lee and Demer 2014) are shown in Table 2. The  $TS$  and  $\theta$  for these live cuttlefish were measured simultaneously using a split-beam echo sounder and a CCTV camera system, respectively and the ( $\langle\theta\rangle$ ) and  $S_\theta$  values were used in estimating the tilt-averaged  $TS$  from the  $TS$  functions of the corresponding cuttlebone.

In the 70 kHz experiments, the mean tilt angles of 19 live cuttlefish varied from  $-3.51^\circ$  to  $-1.05^\circ$  (mean  $-2.31^\circ$ ,



**Fig. 2** Comparison of the  $TS$  functions for cuttlebone ( $L_b = 15.2$  cm,  $W_b = 29.3$  g) measured as a function of tilt angle at 70 (dash line) and 120 kHz (solid line). The precise dorsal-aspect orientation is defined by the angle 0°, and the precise head-down and head-up orientations are defined by angles  $-90^\circ$  and  $90^\circ$ , respectively

**Table 1** Biological characteristics of the corresponding cuttlebone and the body of 19 live cuttlefishes used in the *TS* measurements

Specimen No.	Cuttlefish		Cuttlebone			
	Length <sup>a</sup> (mm)	Weight (g)	Length (mm)	Weight (g)	Width (mm)	Thickness (mm)
1	194	550	185	41.2	63.0	14.8
2	176	435	172	41.6	61.4	15.6
3	165	520	159	31.9	68.0	14.3
4	178	510	173	39.0	66.7	16.8
5	182	643	175	47.9	64.4	16.4
6	174	565	169	33.4	61.0	15.1
7	164	370	155	37.4	58.1	18.0
8	176	512	171	45.3	68.0	16.4
9	158	335	152	29.3	59.8	14.9
10	203	720	195	47.9	66.0	17.2
11	161	475	158	31.3	55.0	13.6
12	156	450	151	31.8	59.0	15.0
13	166	420	161	33.6	62.9	15.5
14	172	530	166	35.9	63.2	15.3
15	177	645	173	48.8	62.0	16.6
16	176	675	173	42.4	59.3	17.8
17	197	645	191	53.2	69.0	16.4
18	160	475	155	30.1	55.0	13.9
19	169	545	163	35.1	63.0	15.5
mean	173.9	527.4	168.3	38.8	62.4	15.7

<sup>a</sup> The length of cuttlefish is a dorsal mantle length

head-down), while the standard deviation varied from 2.32° to 12.64° (mean 6.56°). At 120 kHz, the mean tilt angles varied from -5.11° to -0.73° (mean -3.15°), while the standard deviation varied from 2.33° to 6.86° (mean 4.74°).

**Target strength models**

To compare the *TS* of cuttlebone with that of live cuttlefish, two *TS* values, such as the maximum *TS* (*TS<sub>m</sub>*) and the tilt-averaged *TS* (*<TS<sub>b</sub>>*) in the dorsal-aspect orientation of the cuttlebone, were estimated. First, the *TS<sub>m</sub>* was obtained directly from the measured *TS* functions. Next, the *<TS<sub>b</sub>>* was calculated by using the probability density function *f*(*θ*) of tilt angle *θ*, with mean *θ* (*<θ>*) and standard deviation *S<sub>θ</sub>*, according to Eqs. (1) and (2) (Foote 1980a, 1980b; Pena and Foote 2008):

$$\langle \sigma \rangle = \int \sigma(\theta)f(\theta) d\theta \tag{1}$$

$$\langle TS_b \rangle = 10 \log(\langle \sigma \rangle / 4\pi) \tag{2}$$

where *θ* is the tilt angle defined as the angle made by the cuttlebone centerline with the horizontal, *σ*(*θ*) is the backscattering cross section of tilt angle *θ* and the tilt-angle distribution *f*(*θ*) was assumed to be a truncated

normal distribution function. For each cuttlebone, the *<TS<sub>b</sub>>* was computed over the range *<θ>* - 3 *S<sub>θ</sub>* to *<θ>* + 3 *S<sub>θ</sub>* using the mean tilt angle (*<θ>*) with standard deviation (*S<sub>θ</sub>*) indicated in Table 2.

Each dataset of the mean *TS* of cuttlebone and cuttlefish obtained for 19 specimens at 70 and 120 kHz was regressed on specimen length *L* and wavelength *λ* according to the empirical equation. First, to establish empirical single-frequency relationships between the *<TS>* and the corresponding *L*, the dataset for each frequency was independently fit, in the least-squares sense, to (Benoit-Bird et al. 2008; Conti and Demer. 2003; Demer and Martin 1995; Foote 1987; Goddard and Welsby 1986; Imaizumi et al. 2008; Kang et al. 2005; Sawada et al. 2011):

$$TS = m \log_{10} L + b \tag{3}$$

where *L* is the specimen length (cm), *m* is the slope of the regression line, and *b* is the intercept of the regression line on the *TS* axis.

Next, the datasets from both frequencies were combined to obtain a relationship for a wider range of specimen lengths (*L*) and wavelengths (*λ*):

**Table 2** Mean tilt angles ( $\langle\theta\rangle$ ) with standard deviations ( $S_\theta$ ) used in estimating the mean  $TS$  of cuttlebone at 70 and 120 kHz (Lee and Demer 2014). The  $TS$  and  $\theta$  for live cuttlefish were simultaneously measured by a split-beam echo sounder and a CCTV system, respectively

Specimen No.	70 kHz			120 kHz		
	M. tilt angle (deg)	Standard dev. (deg)	$N$	M. tilt angle (deg)	Standard dev. (deg)	$N$
1	-3.08	12.64	14	-3.15	3.27	16
2	-1.71	6.21	15	-3.01	5.46	15
3	-2.96	7.39	15	-4.77	6.23	15
4	-3.01	9.19	15	-2.01	2.93	15
5	-2.29	2.32	15	-2.29	2.33	15
6	-1.93	3.83	15	-3.03	4.99	15
7	-1.75	5.41	15	-4.23	6.45	15
8	-2.71	9.61	14	-4.87	3.91	14
9	-2.71	5.99	15	-3.25	5.49	15
10	-1.17	3.37	15	-5.11	4.10	15
11	-2.39	5.28	15	-4.61	5.76	15
12	-1.05	6.76	15	-2.37	5.67	15
13	-3.51	8.52	15	-4.55	4.46	15
14	-1.21	3.63	15	-0.73	5.24	15
15	-1.91	6.84	15	-2.39	3.03	15
16	-1.71	6.44	15	-1.43	5.56	15
17	-3.27	6.53	15	-2.77	6.86	15
18	-2.97	6.17	15	-3.07	4.71	15
19	-2.61	8.56	15	-2.13	3.68	15
mean	-2.31	6.56		-3.15	4.74	

$$TS = a \log_{10} L + b \log_{10} \lambda + c \tag{4}$$

where  $L$  is the specimen length (m),  $\lambda$  is the acoustic wavelength (m), and  $a, b, c$  are the fitted coefficients (Love 1969, 1971; McClatchie et al. 1996, 2003).

The mean  $TS$  ( $\langle TS_c \rangle$ ) of live cuttlefish was derived from the results of  $TS$  measurements of the same specimen listed in Table 1 and described fully in our earlier study (Lee and Demer 2014). The influence of cuttlebone on the cuttlefish  $TS$  ( $\langle TS_c \rangle$ ) was analyzed by estimating the difference between these mean  $TS$  values and by comparing the  $TS$ -length relationships for the corresponding cuttlebone and the cuttlefish at 70 and 120 kHz.

**Results**

The  $\langle TS_b \rangle$  of 19 cuttlebones were plotted separately for 70 and 120 kHz versus cuttlebone length  $L_b$ , overlaid on the regressions of Eq. (3) (Figs. 3 and 4).

At 70 kHz,

$$TS = 22.03 \log_{10}(L_b \text{ in cm}) - 60.72, \tag{5}$$

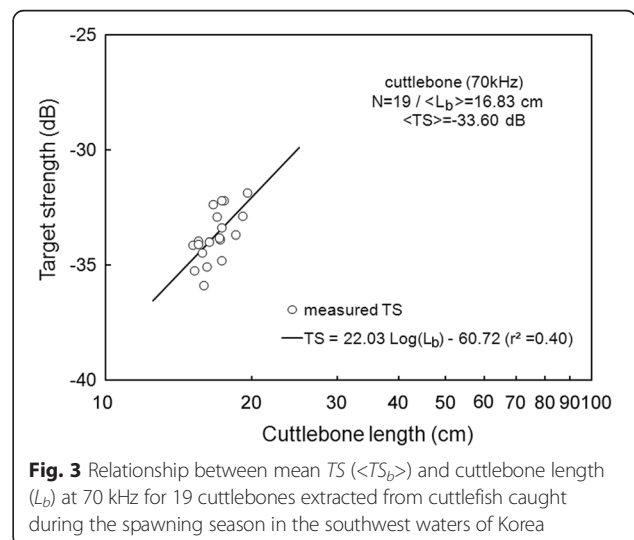
( $r^2 = 0.40, N = 19, P < 0.01$ ).

At 120 kHz,

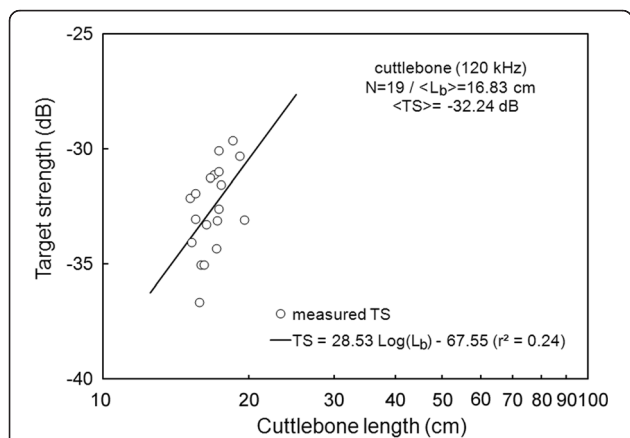
$$TS = 28.53 \log_{10}(L_b \text{ in cm}) - 67.55 \tag{6}$$

( $r^2 = 0.24, N = 19, P < 0.05$ ).

The mean  $\langle TS_b \rangle$  at 70 kHz was -33.60 dB, 1.36 dB lower than that at 120 kHz (-32.24 dB). The mean  $\langle TS_b \rangle$  at 70 kHz was 0.30 dB higher than that indicated by Eq. (5) and the mean  $\langle TS_b \rangle$  at 120 kHz was 0.33 dB higher



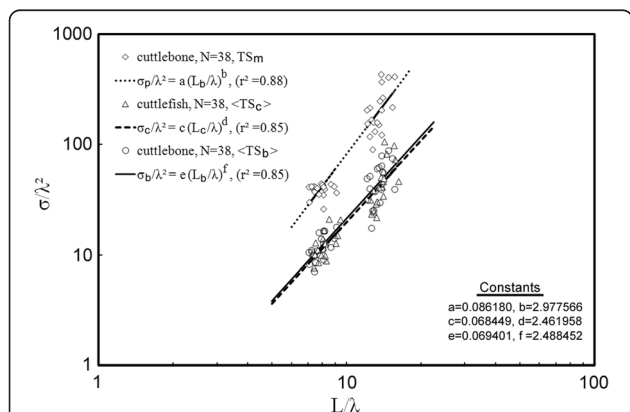
**Fig. 3** Relationship between mean  $TS$  ( $\langle TS_b \rangle$ ) and cuttlebone length ( $L_b$ ) at 70 kHz for 19 cuttlebones extracted from cuttlefish caught during the spawning season in the southwest waters of Korea



**Fig. 4** Relationship between mean  $TS$  ( $\langle TS_b \rangle$ ) and cuttlebone length ( $L_b$ ) at 120 kHz for 19 cuttlebones extracted from cuttlefish caught during the spawning season in the southwest waters of Korea

than that indicated by Eq. (6). The difference between the slopes of the regressions for these frequencies was 6.5, and the intercept at 70 kHz was 6.83 dB higher than that at 120 kHz (Eqs. 5 and 6).

For 70 and 120 kHz combined, the 38 measurements of  $\langle TS_b \rangle$  and  $TS_m$  were transformed to mean scattering cross-sectional areas ( $\sigma$ ;  $m^2$ ) and  $\sigma^2/\lambda$  was plotted versus  $L/\lambda$  (Fig. 5). In Fig. 5, the  $TS_m$  in the dorsal-aspect orientation of cuttlebone was derived by simple extraction from the  $TS$  function measured as a function of tilt angle. The mean  $TS$  ( $\langle TS_c \rangle$ ) of live cuttlefish was obtained from the results of  $TS$  measurements of the



**Fig. 5** Comparison of the relationships between  $\sigma/\lambda^2$  and  $L/\lambda$  for each dataset of cuttlebone and cuttlefish (Lee and Demer 2014) obtained by combining 120 kHz data (Fig. 4) with 70 kHz data (Fig. 3), where  $\sigma_p$ ,  $\sigma_b$  and  $\sigma_c$  are scattering cross-sectional areas ( $m^2$ ) corresponding to the maximum  $TS$  ( $TS_m$ ) and the mean  $TS$  ( $\langle TS_b \rangle$ ) of cuttlebone, and the mean  $TS$  ( $\langle TS_c \rangle$ ) of cuttlefish, respectively.  $L_b$  and  $L_c$  is the lengths (m) of cuttlebone and cuttlefish, respectively and  $\lambda$  is the acoustic wavelength (m). The  $TS$ - $L$  relationships for cuttlebone and cuttlefish was converted from the relationships between  $\sigma/\lambda^2$  and  $L/\lambda$ , respectively

specimens listed in Table 1 and described fully in our earlier study (Lee and Demer 2014).

In this wavelength-normalized form, the  $TS_m$ ,  $\langle TS_b \rangle$ , and  $\langle TS_c \rangle$  values of cuttlebone are comparable between frequencies:

$$\sigma_p/\lambda^2 = 0.086180 \left( L_b/\lambda \right)^{2.977566} \quad (7)$$

$$(r^2 = 0.88, N = 38, P < 0.01)$$

for  $TS_m$ ,

$$\sigma_b/\lambda^2 = 0.069401 \left( L_b/\lambda \right)^{2.486144} \quad (8)$$

$$(r^2 = 0.85, N = 38, P < 0.01)$$

for  $\langle TS_b \rangle$ , and

$$\sigma_c/\lambda^2 = 0.068449 \left( L_c/\lambda \right)^{2.461958} \quad (9)$$

$$(r^2 = 0.85, N = 38, P < 0.01)$$

for  $\langle TS_c \rangle$ , where  $\sigma_p$ ,  $\sigma_b$ , and  $\sigma_c$  are scattering cross-sectional areas ( $m^2$ ) corresponding to the  $TS_m$  and  $\langle TS_b \rangle$  of cuttlebone and the  $\langle TS_c \rangle$  of cuttlefish, respectively.

Using Eq. (4), the predicted  $TS$ 's of an individual specimen of cuttlebone and cuttlefish are indicated by:

$$TS_p = 29.78 \log_{10} L_b - 9.78 \log_{10} \lambda - 21.64 \quad (10)$$

for the predicted value ( $TS_p$ ) of  $TS_m$ ,

$$TS_b = 24.86 \log_{10} L_b - 4.86 \log_{10} \lambda - 22.58 \quad (11)$$

for the predicted value ( $TS_b$ ) of  $\langle TS_b \rangle$ , and

$$TS_c = 24.62 \log_{10} L_c - 4.62 \log_{10} \lambda - 22.64 \quad (12)$$

for the predicted value ( $TS_c$ ) of  $\langle TS_c \rangle$ , where  $L_b$  and  $L_c$  are the length of cuttlebone (m) and the mantle length of cuttlefish (m), respectively and  $\lambda$  is the wavelength (m).

The mean  $TS_m$  values were  $-28.45$  dB at 70 kHz and  $-25.59$  dB at 120 kHz, respectively. These mean  $TS_m$  values were 0.09 dB at 70 kHz and 0.71 dB at 120 kHz higher than those predicted by Eq. (10). The mean  $\langle TS_b \rangle$  values were  $-33.60$  dB at 70 kHz and  $-32.24$  dB at 120 kHz. These mean  $\langle TS_b \rangle$  values were 0.11 dB at 70 kHz and 0.33 dB at 120 kHz higher than those predicted by Eq. (11). The differences between the mean  $TS_m$  and the mean  $\langle TS_b \rangle$  were 5.14 dB at 70 kHz and 6.65 dB at 120 kHz. The mean  $\langle TS_c \rangle$  values were  $-33.41$  dB at 70 kHz and  $-32.20$  dB at 120 kHz. These mean  $\langle TS_c \rangle$  values were 0.23 dB at 70 kHz and 0.35 dB at 120 kHz higher than that predicted by Eq. (12). Furthermore, for 70 and 120 kHz combined, the mean  $\langle TS_c \rangle$  value was  $-32.86$  dB, 0.11 dB higher than the mean  $\langle TS_b \rangle$  value ( $-32.87$  dB). On the other hand, the mean  $\langle TS_c \rangle$

predicted by Eq. (12) was  $-33.06$  dB,  $0.04$  dB higher than the mean  $\langle TS_b \rangle$  predicted by Eq. (11) ( $-33.10$  dB).

Accordingly, the contribution of cuttlebone to cuttlefish  $TS$  determined by the predicted results was slightly larger than that by the measured results. These results suggest that the cuttlebone is fully responsible for the  $TS$  of cuttlefish and the contribution is estimated to be more than 99 % of the total echo strength.

### Discussion

An example of the 70 and 120 kHz echograms recorded as a function of tilt angle, as the cuttlebone is rotated from the spine-on aspect ( $-90^\circ$ ) toward the broadside incidence of the dorsal surface in the pitch plane, is shown in Fig. 5. At spine-on and head-on aspects, there was very weak scattering, and as the cuttlebone was approached from the spine-on aspect toward the broadside orientation, the scattering gradually increased. These angular and frequency dependences of acoustic scattering may allow the cuttlefish to be distinguishable from other fish species, which may be expected to have different responses at these frequencies. In particular, the angular dependence on the backscattering in the dorsal plane of the cuttlebone must be accounted for in relation to the improvement of the fish-sizing accuracy of split-beam echo sounders operating at these frequencies. It is also important to note that the tilt-angle dependence of the echo response in Fig. 6 is extremely complex due to the constructive and destructive interference effects of the backscattering signals generated by internal cuttlebone chambers.

In our previous study (Lee and Demer 2014), the orientation for freely swimming cuttlefish was slightly

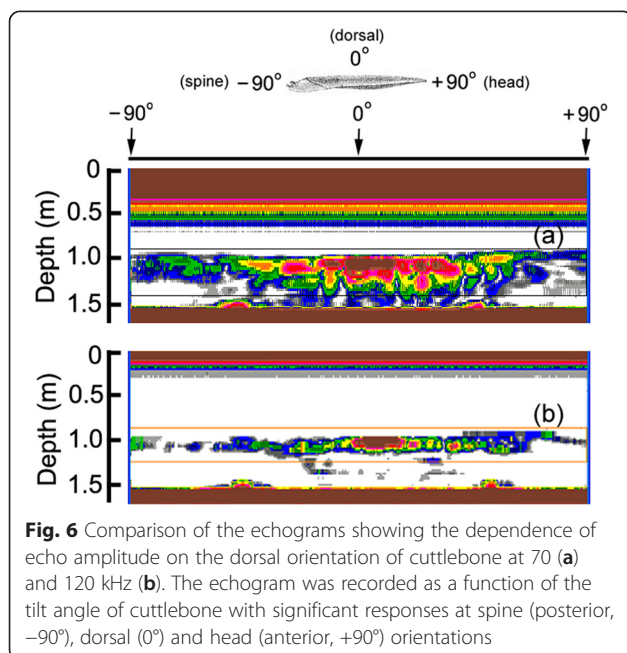
angled head-down relative to the medial axis of the cuttlefish. The strongest backscattering in Fig. 6 was predicted to occur when the cuttlebone surface closest to the sound source is orthogonal to the transducer. However, because of the complexity of the chamber structure, density and curvature of the dorsal surface, the strong echo amplitudes in the echograms for 70 and 120 kHz occurred at slightly head-up aspects (positive tilt-angles).

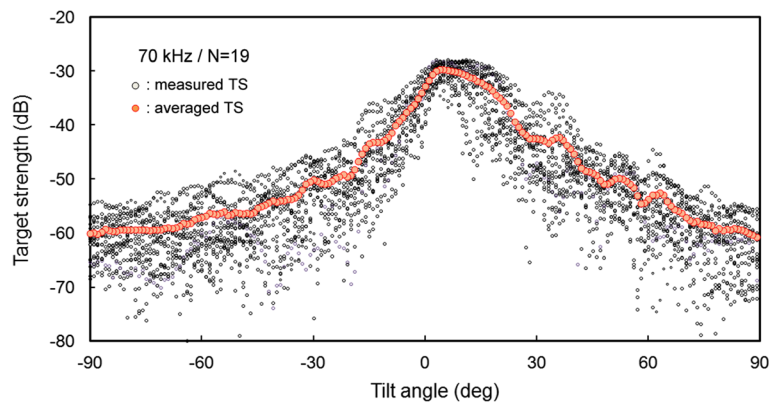
The measured  $TS$  functions, interpolated at  $1^\circ$  intervals, for 70 and 120 kHz are shown in Figs. 7 and 8, respectively; the tilt-averaged  $TS$  functions for all 19 cuttlebones were overlaid on the plot. In Figs. 7 and 8, a positive tilt angle indicates a head-up posture and a negative tilt angle indicates a head-down posture. The strongest responses were observed at slightly head-up aspects between  $1^\circ$  and  $14^\circ$  at 70 kHz and between  $2^\circ$  and  $10^\circ$  at 120 kHz, and weak responses of approximately  $-60$  dB were observed near the spine-on ( $-90^\circ$  aspect) and head-on ( $+90^\circ$  aspect) orientations.

For each cuttlebone, these measured  $TS$  functions were used to calculate the mean  $TS$  over the range  $[\langle \theta \rangle - 3 S_\theta, \langle \theta \rangle + 3 S_\theta]$  from head-down to head-up orientations by Foote's method (Foote 1980a, 1980b; Pena and Foote 2008). A comparison of the tilt-averaged  $TS$  functions of cuttlebone at 70 and 120 kHz is shown in Fig. 9. The tilt-averaged  $TS$  function for 120 kHz showed a strong directivity pattern with higher, narrower peaks and deeper nulls than for 70 kHz, and these  $TS$  patterns were essentially unimodal with the dominant peaks at slightly positive aspects; the tails in the anterior and posterior orientations extended down to  $\sim -60$  dB. It appeared that the tilt-averaged  $TS$  function for 120 kHz exhibited a wider pattern near the peak than at 70 kHz (Fig. 9), but the broadening was due to the overlapping of  $TS$  patterns with different tilt angles for the peak positions (Figs. 7 and 8). The peak  $TS$  values in the tilt-averaged  $TS$  functions were  $-29.6$  dB at a tilt angle of  $+5^\circ$  for 70 kHz and  $-27.5$  dB at a tilt angle of  $+3^\circ$  for 120 kHz, respectively and the peak  $TS$  at 120 kHz was 2.1 dB higher than at 70 kHz.

Cuttlebone is bilaterally symmetrical in shape and derived from the juxtaposition of four parts: the outer cone, inner cone, phragmocone and spine. The dorsal surface of cuttlebone is evenly convex in outline but the anterior, median and posterior parts have slightly different curvatures (Neige 2003). Due to these morphological characteristics of cuttlebone, the dependence on the orientation of the cuttlebone  $TS$  is sensitive to the incidence direction (Figs. 7 and 8).

A comparison of the mean  $TS$  of cuttlefish with the mean  $TS$  of cuttlebone is shown in Fig. 10. A comparison of the measured and predicted contributions of cuttlebone to cuttlefish  $TS$  is shown in Table 3. In



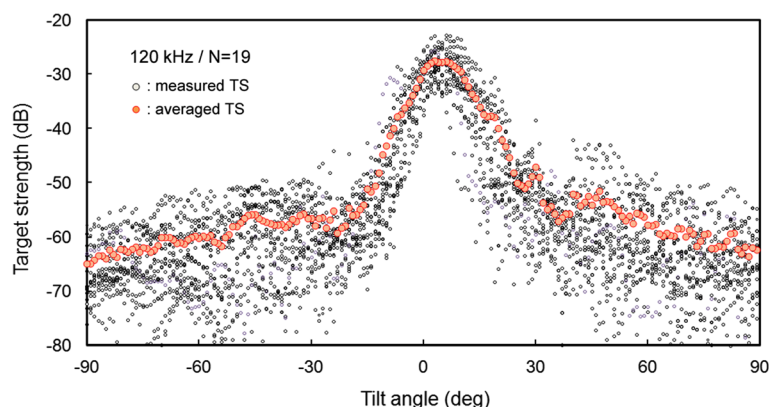


**Fig. 7** *TS* functions (open circle) for all 19 cuttlebone measured as a function of tilt angle over the angle range  $[-90^\circ, 90^\circ]$  from head-down to head-up orientations of the dorsal plane at 70 kHz. The tilt-averaged *TS* function (solid circle) was overlaid on the plot

Table 3, the contributions are indicated as the differences between the mean *TS* values that are described within the 95 % confidence limits. In Fig. 10 and Table 3, the mean *TS* values measured using the combined dataset of all 38 specimens for 70 and 120 kHz were  $-32.76$  dB for cuttlefish and  $-32.87$  dB for cuttlebone; i.e., the mean *TS* of cuttlefish was 0.11 dB higher than that of cuttlebone. On the other hand, the mean *TS* values predicted by regressions of the combined dataset of all 38 specimens for 70 and 120 kHz were  $-33.06$  dB for cuttlefish and  $-33.10$  dB for cuttlebone; i.e., the mean *TS* of cuttlefish was 0.04 dB higher than that of cuttlebone. Accordingly, the contribution of cuttlebone to cuttlefish *TS* in the predicted results was slightly larger than in the measured results (Table 3). Furthermore, the measured mean *TS* values of cuttlefish and cuttlebone for a single frequency of 70 kHz were  $-33.41$  and  $-33.60$  dB, respectively; a 0.19 dB difference. The measured mean *TS* values of cuttlefish and cuttlebone at a

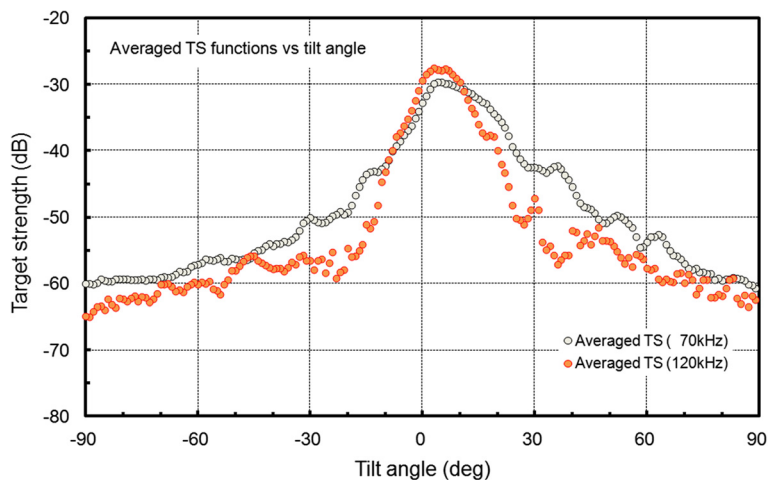
single frequency of 120 kHz were  $-33.41$  and  $-33.60$  dB, respectively; a 0.19 dB difference. That is, the contribution of cuttlebone at 120 kHz was 0.15 dB higher than at 70 kHz (Table 3). On the other hand, the predicted mean *TS* values of cuttlefish and cuttlebone at a single frequency of 70 kHz were  $-33.63$  and  $-33.71$  dB, respectively; a 0.08 dB difference. The predicted mean *TS* values of cuttlefish and cuttlebone at a single frequency of 120 kHz were  $-32.55$  and  $-32.60$  dB, respectively, a 0.02 dB difference. That is, the contribution of cuttlebone at 120 kHz was 0.06 dB higher than at 70 kHz (Table 3).

The slopes of the regressions for a single frequency in this study were estimated to be  $22.03$  [95 % confidence interval (CI),  $22.03 \pm 13.87$ ,  $P < 0.01$ ] at 70 kHz and  $28.53$  [95 % CI,  $28.53 \pm 26.29$ ,  $P < 0.05$ ] at 120 kHz [Eqs. (5) and (6)]. These results suggest that the mean *TS* of cuttlebone varies with approximately the square power of the length at 70 and 120 kHz. The intercept [95 % CI,



**Fig. 8** *TS* functions (open circle) for all 19 cuttlebone measured as a function of tilt angle over the angle range  $[-90^\circ, 90^\circ]$  from head-down to head-up orientations of the dorsal plane at 120 kHz. The tilt-averaged *TS* function (solid circle) was overlaid on the plot





**Fig. 9** Comparison of the tilt-averaged TS functions of cuttlebone obtained at 70 (open circle) and 120 kHz (solid circle)

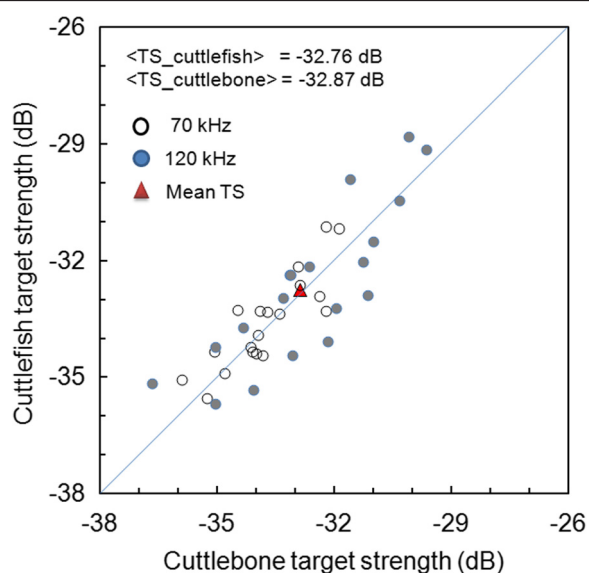
-60.72 ± 17.00 dB,  $P < 0.01$ ] of the regression line at 70 kHz was 6.83 dB higher than at 120 kHz [95 % CI, -67.55 ± 32.21 dB,  $P < 0.01$ ].

According to Simmonds and MacLennan (2005), the slope ( $m$ ) and intercept ( $b$ ) of cuttlefish vary widely versus fish species and commonly have values between 18 and 30 and 60 and 80, respectively. The slope and intercept in this study were within these ranges, although the determination coefficient ( $r^2$ ) indicated relatively low values of  $r^2 = 0.40$  at 70 kHz and  $r^2 = 0.24$  at 120 kHz. Compared to our earlier study (Lee and Demer 2014), the slopes for cuttlebone were 2.64 at 70 kHz and 12.06

at 120 kHz, lower than those of cuttlefish, and the intercepts for cuttlebone were 3.31 dB at 70 kHz and 15.41 dB at 120 kHz, higher than those of cuttlefish.

The chi-squared test of independence (CSTI, 99 % confidence level) for the  $TS_m$  and the  $\langle TS_b \rangle$  values at 70 and 120 kHz showed that the  $TS_m$  and the  $\langle TS_b \rangle$  values of cuttlebone at these two frequencies were independent ( $P > 0.01$ ). Accordingly, to compare the  $TS_m$  and the  $\langle TS_b \rangle$  values measured at multiple frequencies, a non-dimensional representation may be used (McClatchie et al. 1996; McClatchie et al. 2003, this study). In this study, the 38 wavelength-normalized  $TS_m$  and  $\langle TS_b \rangle$  values measured at two frequencies from 19 cuttlebones were compared and showed length-dependent scattering [e.g., Eqs. (10), (11) and (12)]. This formulation allowed twice the number of measurements (38 vs. 19) to be combined in the regression (Love 1969, 1971), which resulted in a considerably better fit [ $r^2 = 0.88$  in Eq. (10),  $r^2 = 0.85$  in Eq. (11), and  $r^2 = 0.85$  in Eq. (12)] (Fig. 5). The fitted coefficient  $a$ ,  $b$  and  $c$  values for the regressions of Eqs. (4) and (11) were 24.86 [95 % CI, 24.86 ± 3.57,  $P < 0.01$ ], -4.86 [95 % CI, -4.86 ± 3.57,  $P < 0.01$ ], and -22.58 [95 % CI, -22.58 ± 3.64,  $P < 0.01$ ], respectively. In Fig. 5, the regression of the maximum TS ( $TS_m$ ), which is within the 95 % confidence limit, was ~5 dB higher than that of mean TS ( $\langle TS_b \rangle$ ). Furthermore, at both frequencies, the contributions of the measured results were similar to those of the predicted results (Table 3). It is important to note that if the truncated limit of the tilt-angle distribution in the averaging operation by Foote's method (Foote 1980a, 1980b; Pena and Foote 2008) is controlled, the contribution may be altered to some extent.

The TS of cuttlefish is expected to be markedly less depth-dependent than that of swimbladder fish because the buoyancy mechanism of cuttlebone, unlike the fish swimbladder, is almost independent of depth during



**Fig. 10** Relationship between the measured TS values for all 38 specimen of cuttlebone and cuttlefish at 70 (open circle) and 120 kHz (solid circle). Comparison of the mean TS ( $\langle TS_b \rangle$ ) of cuttlefish with the mean TS ( $\langle TS_b \rangle$ ) of cuttlebone was indicated as a solid triangle. Solid line indicates a reference line for comparison

**Table 3** Comparison of the measured and predicted contributions of cuttlebone on the cuttlefish *TS* at 70 and 120 kHz. The contributions are indicated as the differences between the mean *TS* values that are described within the 95 % confidence limits

Frequency (kHz)	Measured results			Predicted results		
	Cuttlefish (dB)	Cuttlebone <i>TS</i> (dB)	Diff. (dB)	Cuttlefish <i>TS</i> (dB)	Cuttlebone <i>TS</i> (dB)	Diff. (dB)
70	-33.41	-33.60	0.19	-33.63	-33.71	0.08
120	-32.20	-32.24	0.04	-32.55	-32.60	0.02
mean	-32.76	-32.87	0.11	-33.06	-33.10	0.04

vertical movements (Denton and Gilpin-Brown 1961; Denton et al. 1961; Denton and Taylor 1964). Knudsen and Gjelland (2004) reported that at least some coregonid species are capable of filling the swimbladder without access to the surface during the diel vertical migration and that *TS* did not decrease with depth. This swimbladder volume compensation in coregonids is compared to buoyancy regulation by the cuttlebone in cuttlefish. Generally, the change in the surface area of the swimbladder caused by the change in swimbladder volume affects *TS*, but because the dorsal surface of cuttlebone is unaffected by depth, the depth effect of cuttlebone on cuttlefish *TS* is not expected to be affected like the swimbladder of fish. Instead of having a flexible swimbladder like a fish, cuttlefish have a cuttlebone, which has a rigid structure, for buoyancy control. The cuttlebone is divided by many thin, chitinous partitions, which separate gas-filled anterior chambers and fluid-filled posterior chambers of approximately periodic microstructure (Denton and Gilpin-Brown 1961; Denton et al. 1961; Denton and Taylor 1964; Neige 2003; Cadman et al. 2010a, 2010b; Chen et al. 2011). Unlike the swim bladder of fish, cuttlebone is unpressurized, so its volume is not altered markedly as the animal changes depth (Denton and Gilpin-Brown 1961; Denton et al. 1961; Denton and Taylor 1964), and no adjustments to the buoyancy system are necessary during vertical movements (Sherrard 2000).

Generally, the fish *TS* is proportional to the difference in density between the insonified fish target and the surrounding water (Simmonds and MacLennan 2005), and the main source of backscatter is expected to be proportional to the size of the swimbladder, which accounts for at least 90 % of echo energy (Foote 1980a, 1980b, 1985; Foote and Ona 1985). The impedance of gas-filled organs, such as the swimbladder and cuttlebone, differs considerably from that of seawater and other fish tissues, and the scattering contribution of cuttlebone is comparable to that of an air-filled swimbladder. However, in cuttlefish, the problems of pressure changes are avoided by enclosing the gas in the cuttlebone, the volume of which is unaffected by changes in depth and which contains many chambers, some filled with gas and some with liquid. The overall density of the cuttlebone varies between ~0.5 and 0.7, and is controlled by regulating its

liquid content (Denton and Gilpin-Brown 1961; Denton et al. 1961; Denton and Taylor 1964). Accordingly, the acoustic scattering by cuttlefish is expected to fluctuate in proportion with changes in the overall density of cuttlebone. Madsen et al. (2007) reported that the muscular mantle and fins of the common squid are the dominant scatterers, and that the hard parts—such as beak, eyes and pen—contribute little to the *TS* of squid, at least for frequencies representative of the clicks of most teutophageous toothed whales. This suggests that the acoustic interference of the muscular mantle, fins and cuttlebone in freely swimming cuttlefish are complexly generated based on frequency.

In this study, the *TS* of cuttlebone was measured and analyzed as a function of length only; however, the *TS* may actually be more sensitive to the dorsal surface area (or volume) of cuttlebone rather than the length. Based on a comparison of the *TS-L* relationships for the corresponding cuttlebone and live cuttlefish for 19 specimens, the contribution of cuttlebone to the backscattering echo strength of cuttlefish was estimated to be at least 99 %. Moreover, the cuttlebone volume (or surface area) may have a greater influence on cuttlefish *TS* than the length, because the proportion of cuttlebone volume as a fraction of the total body volume of cuttlefish (~9.3 %) is almost twofold that of the swimbladder of fish (~5 %) (Denton and Gilpin-Brown 1961; Denton et al. 1961; Denton and Taylor 1964). The relationship between cuttlebone volume and cuttlefish *TS* may be complicated by the complex microstructure of the gas-filled internal shell of the cuttlebone. However, the effects of the morphological and material parameters of cuttlebone—such as length, width, height, density change and curvature of the dorsal surface—must be analyzed to quantitatively estimate the influence of cuttlebone on cuttlefish *TS*. This will be the subject of a future study.

## Conclusions

The mean *TS* values of cuttlebone were 0.19 and 0.04 dB lower than those of cuttlefish at 70 and 120 kHz, respectively. The contribution of cuttlebone to the cuttlefish *TS* determined by the measured results was slightly greater than that by the predicted results. From these results, we concluded that cuttlebone is responsible for the *TS* of

cuttlefish, and the contribution is estimated to be at least 99 % of the total echo strength.

#### Competing interests

The author declares that he has no competing interests.

#### Author's contribution

DL carried out the experiment, wrote the manuscripts and performed the data analysis. The author approved the final version of the manuscript.

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